Serial No. Docket No. 10/762,559

K06-165935M/TBS

(NGB.353)

## **AMENDMENTS TO THE CLAIMS:**

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## Please amend the claims as follows:

1. (Currently Amended) A steel for use in a high strength pinion shaft made by a method comprising:

hot rolling at a temperature of 700°C to 850°C under a draft ratio at an area reduction of 10% or more; and

high frequency hardening the steel, said steel comprising:

0.45wt% - 0.55wt% C;

0.21wt%-0.45wt% Si;

0.50wt% - 1.20wt% Mn;

0.025wt% or less P;

0.025wt% or less S;

0.15wt% - 0.25wt% Mo;

0.0005wt% - 0.005wt% B;

0.005wt% - <del>0.010wt% Ti;</del> 0.10wt% Ti;

0.015wt% or less N; and

a balance comprising Fe and impurities,

wherein the steel comprises a 3-phase texture of ferrite + pearlite + bainite,

wherein  $0.80 \le \text{Ceq} \le 0.95$ , where  $\text{Ceq} = \text{C} + 0.07 \times \text{Si} + 0.16 \times \text{Mn} + 0.20 \times \text{Cr} + 0.72 \times \text{Mo}$ .

wherein f value  $\leq$  1.0, where f value = 2.78-3.2×C + 0.05×Si - 0.60×Mn - 0.55×Cu -

 $0.80 \times Ni - 0.75 \times Cr$ , and

wherein the steel is devoid of Cr, Cu, Ni and Al.

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- 2. (Canceled)
- 3. (Currently Amended) A steel for use in a high strength pinion shaft according to claim 1, further comprising one or more of 0.20wt% or less Nb, 0.20wt% or less Ta, and 0.10wt% or less Zr and 0.10wt% or less Al instead of a portion of said Fe.
- 4. (Canceled)
- 5. (Currently Amended) A steel for use in a high strength pinion shaft <u>made by a method</u> comprising:

hot rolling at a temperature of 700°C to 850°C under a draft ratio at an area reduction of 10% or more; and

high frequency hardening the steel, said steel comprising:

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0.45wt% - 0.55wt% C;
0.21wt%-0.45wt% Si;
0.50wt% - 1.20wt% Mn;
0.025wt% or less P;
0.025wt% or less S;
0.15wt% - 0.25wt% Mo;
0.0005wt% - 0.005wt% B;
0.005wt% - 0.010wt% Ti; 0.10wt% Ti;
0.015wt% or less N; and
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a balance comprising Fe and impurities,

wherein the steel, having been hot rolled, comprises a 3-phase texture of ferrite + pearlite + bainite,

wherein a ferrite area ratio is 40% or less,

wherein a maximum pearlite block size is  $100~\mu m$  or less in a circle-equivalent diameter,

wherein a hardness after hot rolling is 24 to 30 HRC,

wherein a surface hardness after high frequency hardening is 650 HV or higher, wherein an old austenite crystal grain size in a hardened layer is 8 or more in view of grain size number,

 $\frac{\text{wherein } 0.80 \leq \text{Ceq} \leq 0.95, \text{ where } \text{Ceq} = \text{C} + 0.07 \times \text{Si} + 0.16 \times \text{Mn} + 0.20 \times \text{Cr} + 0.72 \times \text{Mo}, }{\text{wherein } \text{f value} \leq 1.0, \text{ where } \text{f value} = 2.78 - 3.2 \times \text{C} + 0.05 \times \text{Si} - 0.60 \times \text{Mn} - 0.55 \times \text{Cu} - 0.80 \times \text{Ni} - 0.75 \times \text{Cr}, }$ 

wherein the steel is devoid of Cr, Cu, Ni and Al.

- 6. (Canceled).
- 7. (Currently Amended) A steel for use in a high strength pinion shaft according to claim 5, further comprising one or more of 0.20wt% or less Nb, 0.20wt% or less Ta, and 0.10wt% or less Zr and 0.10wt% or less Al instead of a portion of said Fe.
- 8. (Canceled)

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9. (Currently Amended) A method of manufacturing a steel for use in a high strength pinion shaft in which a steel comprising:

providing a steel comprising:

0.45wt% - 0.55wt% C;

0.21wt%-0.45wt% Si

0.50wt% - 1.20wt% Mn;

0.025wt% or less P;

0.025wt% or less S;

0.15wt% - 0.25wt% Mo;

0.0005wt% - 0.005wt% B;

0.005wt% - <del>0.010wt% Ti;</del> <u>0.10wt% Ti;</u>

0.015wt% or less N; and

a balance comprising Fe and impurities, is fabricated or worked under a draft ratio at an area reduction of 10% or more, and at a temperature of 850°C or lower,

wherein 0.80 ≤Ceq≤0.95, where Ceq = C + 0.07×Si + 0.16×Mn + 0.20×Cr + 0.72×Mo, wherein f value ≤ 1.0, where  $T_{Tr}$  = 2.78 – 3.2×C + 0.05×Si – 0.60×Mn – 0.55×Cu – 0.80×Ni – 0.75×Cr,

said method comprising hot rolling said steel at a temperature of 700°C to 850°C under a draft ratio at an area reduction of 10% or more to obtain a steel comprising a 3-phase texture of ferrite + pearlite + bainite; and

high frequency hardening the steel, and

wherein the steel is devoid of Cr, Cu, Ni and Al.

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- 10. (Canceled)
- 11. (Currently Amended) A method of manufacturing a steel for use in a high strength pinion shaft according to claim 9, further comprising one or more of 0.20wt% or less Nb, 0.20wt% or less Ta, and 0.10wt% or less Zr and 0.10wt% or less Al instead of a portion of said Fe.
- 12. (Canceled)
- 13. (Previously Presented) A steel for use in a high strength pinion shaft according to claim 1, wherein a ferrite ratio of said steel comprises 40% or less.
- 14. (Previously Presented) A steel for use in a high strength pinion shaft according to claim 1, wherein a hardness of said steel after hot rolling comprises a range of 24 HRC to 30 HRC.
- 15. (Previously Presented) A steel for use in a high strength pinion shaft according to claim 1, wherein a surface hardness of said steel comprises 650 HV or more.
- 16. (Previously Presented) A steel for use in a high strength pinion shaft according to claim 1, wherein said steel comprises an old austenite crystal grain size of 8 or more.
- 17. (Previously Presented) A method of manufacturing a steel for use in a high strength

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pinion shaft according to claim 9, wherein said steel is fabricated or worked under a temperature in a range of 700°C to 850°C.

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- 18. (Previously Presented) A steel for use in a high strength pinion shaft according to claim 1, wherein a torsional strength of said steel comprises 1670 Mpa to 1800 Mpa.
- 19. (Previously Presented) A steel for use in a high strength pinion shaft according to claim 1, wherein a wear loss of said steel comprises 0.002g to 0.004g.
- 20. (Canceled)
- 21. (Canceled)